

Development of Kinematic Criterion for Undercutting Induced Rock Failures

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Abstract

The interlayered soft and hard rocks exhibit difference in weathering rate. This differential weathering leads to various failure modes such as rockfall, rock-slides, plane fall/slide and wedge fall/slide in upper lying hard units, which is eventually induced by the erosion of the underlying weaker lithologies. However, the geometry and orientation of joints in hard rock play an essential role in causing these failures that were not reported previously. The current research focuses on developing a kinematic criterion for these undercutting-induced rock slope failures. In this study, the discontinuity data were gathered from the thirteen cut slopes along the Islamabad-Muzaffarabad Dual carriageway, Pakistan, where the rocks of Murree Formation of Miocene age are exposed. The discontinuity data was analysed in the DIPS software that indicated the three orthogonal joints along the slopes with the bedding of the rock unit dipping into the hill. The horizontal and into the slope orientation of the major joint is generally considered favourable; however, the field evidence is depicted otherwise in the interlayered lithologies. The results of this research showed that the undercutting is more pronounced along gentler bedding joints either into or out of the slope; on the other hand, it has less effect on the slope where the strike is across the hill, dipping on either side at steep to very steep angles.

1. Introduction

The interlayered lithologies are typical in sedimentary origin rocks, resulting from transgression and regression processes (Blatt, 1982; Crook, 1960; J.A. Franklin & Chandra, 1972; Potter et al., 1980; Wood & Deo, 1975). These rocks are commonly present all around the globe and have been reported by Akram et al. (2018); Cano & Tomás (2013); Hussain et al. (2015); Mišćević & Vlastelica (2014); Shakoor &

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Weber (1988); and Zhang et al. (2016). Undercutting due to differential weathering is frequently observed in these rocks (Admassu et al., 2012; Admassu & Shakoor, 2013; Gautam & Shakoor, 2016; Niemann, 2009; Shakoor, 1995; Shakoor & Weber, 1988). The soft blocks of rock such as of shale, claystone, mudstone are more susceptible to weathering and erode at higher rates than the hard lithologies such as of sandstone, siltstone and silt-shale (Dick et al., 1994; Z.A. Erguler & Shakoor, 2009; J.A. Franklin & Chandra, 1972; Heidari et al., 2018; Koncagül & Santi, 1999; Selen et al., 2020). This differential weathering shape overhangs in the upper lying hard lithologies (Shakoor & Rodgers, 1992). The lower-lying soft lithologies stop supporting them due to the higher erosion rate. Hence, it speeds up the movements of planes and wedges, which eventually changes into the falling and sliding mode of blocks. Shakoor & Weber (1988) initially reported such types of rockfall and slide failures. Similarly, the crack initiation in the upper competent block and depth of undercutting is discussed in detail by (Zhang et al., 2016).

The differential weathering is always associated with the slaking nature of rocks, and at a laboratory scale, the slaking nature of rocks is assessed by the slake durability test (ASTM, 2008, 2016; Zeynal Abiddin Erguler & Shakoor, 2009; John A Franklin & Chandra, 1972). However, various tests, such as the jar slake test (Santi, 1998) and the nail penetration test (Özdemir & Erguler, 2021), are used for these lithologies in the field (Zeynal Abiddin Erguler & Shakoor, 2009). Similarly, the methodology to design the ditch to limit the rock falling mode induced in these slopes is discussed by Admassu (2010); Admassu et al. (2012); Admassu & Shakoor (2013). Despite the extensive studies carried out in the line to restrict these undercutting induced failures, however, in the light of kinematic analyses, the failures are not available in the literature. The other kinematic criterion for different failure modes, such as the plane, wedge, and topple, are reported in the literature (Hudson & Harrison, 2000; Wyllie & Mah, 2014). The kinematic criterion for plane failures along slopes is defined as the failure is likely along slopes where one of the joint strike parallel or sub-parallel to the slope face. The dip direction of the failure plane is gentler than that of the slope face. In addition, the friction angle of the rock must be smaller than the dip of the failure plane.

Similarly, the Markland test is commonly used for wedge failures (Markland, 1972, 1974). According to the test, the criterion for the wedge failure along slopes is explained as follows: a wedge should be formed by the two intersecting joints that should daylight on the slope face and marked by the line of intersection. The strike of the line of intersection of two joints must be parallel to the strike of the slope face joint. The dip of the line of intersection should be greater than the friction angle. Lastly, the kinematic criterion for toppling failure is defined as the toppling failure is likely along the slope if the dip direction of the joint plane is parallel or sub-parallel to the dip direction of the slope face. The other joints must dip at steep or very steep angles dipping into the slope. There should be another joint set that defines the height of the block. The most convenient way to study these rock failures along slopes is by drawing the great circles on the stereo nets (Goodman & Shi, 1985; Lisle & Leyshon, 2004). It should be noted that these kinematic criteria are for the slopes where one rock unit is exposed and are not likely to define the failures in interlayered lithologies especially comprising hard and soft lithologies side by side. This study aims to develop a kinematic criterion for undercutting induced failures and identify the region of major rock failure induced by its geometry. In the present research, a similar method of stereographic projection techniques is utilized to define the limits of the undercutting induced rock failures.

2. Geology of the Study Area

This study is carried out along the cut slopes of Islamabad Muzaffarabad Dual Carriageway (IMDC), Pakistan, where the rocks of the Murree Formation of the Miocene age comprise interlayered sandstone /siltstone /silt-shale and shale/ mudstone/ claystone are exposed (Akram et al., 2018; Iqbal & Shah, 1980; Kazmi & Jan, 1997; Shah, 1977) (Figure1). According to the regional geological map of the study area, the sequence of synclines and anticlines are present in the area trending in the northeast-southwest. The

competent rocks comprise sandstone, siltstone, and silty shale, while incompetent units are shale, mudstone, and claystone. The competent rocks are massive to blocky, while incompetent rocks are thinly bedded to laminated. The sandstone of purple to greyish brown with subordinates beds of reddish-brown siltstone, mudstone, and claystone. The Murree Formation is comprised of a monotonous sequence of dark red and purple clay and purple grey and greenish-grey sandstone. The name Murree Formation is designated to the rocks of Mari Group of Wynne (1874), and Murre Series of Pilgrim (1910). The upper contact of Murree Formation is with Kamliyal Foramtion which is transitional, while the lower contact is unconformable. The slaking nature of various rocks units of the formation is variable.

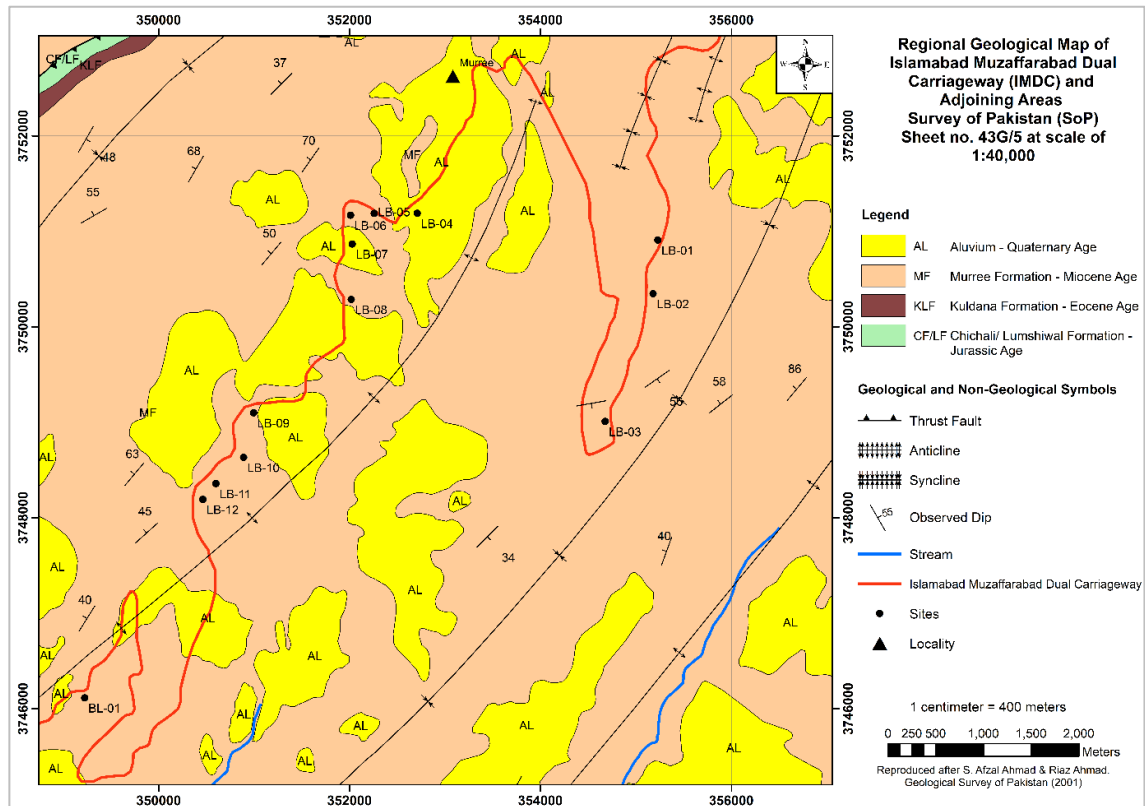


Fig. 1. The geological map of the study area (reproduced after Ahmad & Ahmad 2001).

3. Methodology

The methodology adopted for the current research comprises collecting the field orientation data from various cut slopes using the window and scan line sampling techniques (Cawood et al., 2017; Delaney et al., 2019; Fisher et al., 2014; Piteau & Martin, 1977; Wyllie & Mah, 2004) and collecting samples for friction angle tests. In the field, it is observed that the sub-horizontal to horizontal bedding joint is dipping into the hill throughout the project area with a change in the strike. The sandstone and siltstone are massive to blocky, while shale is thinly bedded to laminated. In addition, the likely state of failure mode was also recorded in the field perform. In the laboratory, the friction angles were determined by tiltmeter test (Alejano et al., 2018; Pérez-Rey et al., 2016). The average friction angle of sandstone and siltstone is 30° with a range from 29° to 31°, whereas the average friction angle of claystone is found to be 25.5° with

a range from 24° to 27° . The Rocscience suite DIPS were used for the interpretation of respective failure modes in the slopes. Akram et al. (2018) previously reported these failure modes with conventional kinematic for plane, wedge and toppling for similar sites. The primary modes of failure were plane and wedge along the slopes, and the toppling mode of failure is absent in the slope. In the light of the field data and observations, laboratory testing and detailed failure results, the kinematic criterion was proposed for the undercutting induced rock failures.

4. Development of Kinematic Criterion

The kinematic criterion was developed based on the field orientation data plotted on the lower hemisphere stereo-net with a fixed and normalized steep slope face of 70° . The orientation data of every window were rotated to this fixed slope face, and the poles of the joints were marked as per the poles plotting on the stereo-nets. The modes of failure observed in the field were used to designate the zone of likely failure on the stereo-net. Based on the analyses, three zones were identified for undercutting induced rock failures (Figure 2). It was observed that the undercutting is more pronounced along gentler bedding joints either into or out of the slope; on the other hand, it has less effect on the slope where the strike is across the hill, dipping on either side at steep to very steep angles. It should be noted that the kinematic criterion is developed for the interlayered lithologies and should be used with precaution for other lithologies.

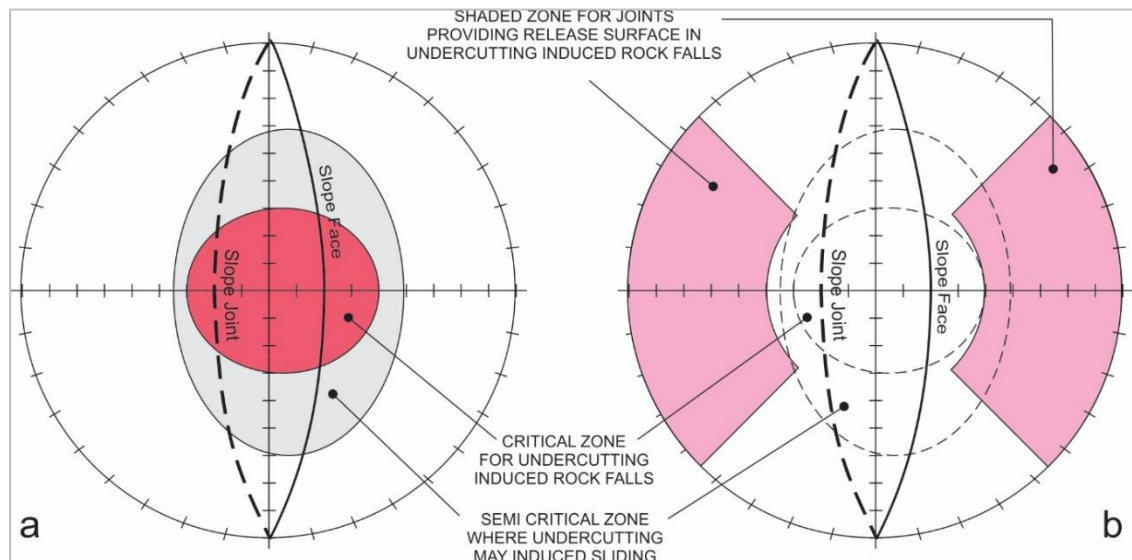


Fig. 2. The proposed criterion for undercutting induced rock failures.

5. Conclusions

The present research was carried out for the development of a kinematic criterion for undercutting induced rock failures that were not identified in the conventional kinematic criterion for plane, wedge and toppling. The kinematic criterion is developed on the lower hemisphere equal area equatorial stereo-net. These three zones can be explained as;

- (1) The undercutting-induced rock fall's critical zone covers the centre of the stereo-net (marked with red colour in Figure 2).
- (2) The Semi-critical zone surrounding the critical zone is in an oval shape, and the likely mode of failure is undercutting induce sliding (marked with grey colour in Figure 2).
- (3) Shaded zone for joints that provide release surface in undercutting induce rockfalls (marked with pink colour in Figure 2).

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